

CADMUS



Minnesota TRM 3.2 Proposed Measure Update Discussion

September 28, 2020

Agenda

Welcome

Schedule

Measures

- Variable speed pool pumps

- Strip curtains

- Water heater jacket insulation

- Lighting controls

- Line voltage smart thermostats

- ECM fan motors

- Evap fan speed controls and motors

Additional items



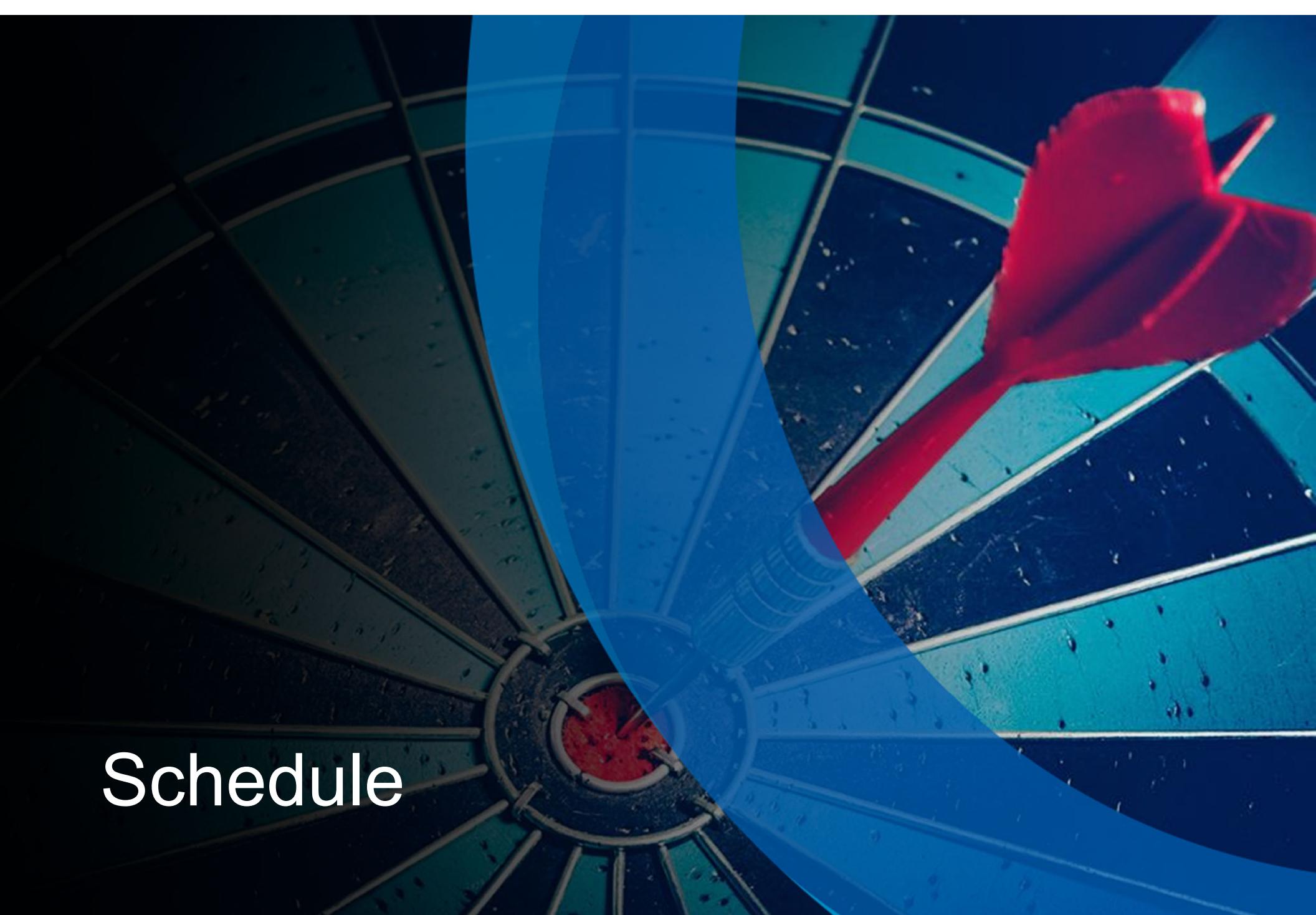
Welcome

CADMUS

Roll Call

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	Carrie Donohue



Schedule

Schedule

Item	Appx. Dates
Measure updates	9/4 - 9/30
Update discussion meeting	9/28
Discussion via e-mail / Huddle	9/28 - 10/16
Draft TRM submitted in eDockets	10/23
eDockets comments due	11/11
eDockets replies due	11/25
Final TRM submitted in eDockets	12/16

- Use time between now and ~10/16 to dial in updates via e-mail + Huddle
- Goal is a draft TRM ~10/23 that requires little modification
- After draft TRM, comments via eDockets only



Measures

Strip curtains

- Update to submitted version: Modify only; required by code
- ΔkWh savings = $\Delta\text{kWh}/\text{SqFt} \times A$
- A = input or default from table

Facility Type	Pre Existing Curtain Condition	Energy Savings (kWh/SqFt)	Demand Reduction (kW/SqFt)	Default Doorway Area (square feet)
Supermarket - Cooler	Existing curtain	37	0.0042	35
	No curtain	108	0.0123	
	Unknown	108	0.0123	
Supermarket - Freezer	Existing curtain	119	0.0136	35
	No curtain	349	0.0398	
	Unknown	349	0.0398	
Convenience Store - Cooler	Existing curtain	5	0.0006	21
	No curtain	20	0.0023	
	Unknown	11	0.0013	
Convenience Store - Freezer	Existing curtain	8	0.0009	21
	No curtain	27	0.0031	

- Originates from 2016 Pennsylvania TRM
 - “All the assumptions in this protocol are based on values that were determined by direct measurement and monitoring of over 100 walk-in units in the 2006-2008 evaluation for the CA Public Utility Commission.”
- Used in WI, AR, and IL as well

Variable speed pool pumps

- Original note was that variable-speed is code, but not quite true.
- $\Delta \text{kWh savings} = V_{\text{POOL}} \times N_{\text{TURNOVERS}} \times \text{Days} \times (1/\text{WEF}_{\text{BASE}} - 1/\text{WEF}_{\text{EFF}})$
- V, N, and Days from 2013 paper by (other) CEE
- Previous: $\text{EF}_{\text{BASE}} = 2 \text{ gal/Wh}$, $\text{EF}_{\text{EFF}} = 8.37$ (avg in CA database)
- New:

Equipment Class			Baseline WEF	
Pool Pump Type	hhp range	Motor phase	Standard	Value Range
Self-priming, w/ filter	hhp < 0.13	single	5.55	5.55
	0.13 ≤ hhp < 0.771		-1.3 × ln(hhp) + 2.9	5.55 at 0.13 hhp 3.24 at 0.77 hhp
	0.771 ≤ hhp < 2.5		-2.3 × ln(hhp) + 6.59	7.16 at 0.771 hhp 4.49 at 2.49 hhp
Non self-priming, w/ filter	hhp < 0.13	any	4.60	4.60
	0.13 ≤ hhp < 2.5		-0.85 × ln(hhp) + 2.87	4.6 at 0.13 hhp 2.09 at 2.49 hhp
Pressure cleaner booster	any	any	0.42	0.42

Mean WEF from ES		
Base	Eff	Count
3.7	10.4	41
6.1	7.7	152
4.6	8.2	8
0.4	0.6	5

- Prefer to list defaults for WEF_{BASE} and WEF_{EFF} ? Table on right.

DHW jacket insulation

- Added electric DHW, changed formula format, checked defaults
- Formula previously read $U \times A$, now reads A / R

Unit kWh Savings per Year =
$$(A_{base} / R_{base} - A_{insul} / R_{insul}) \times (T_{hot} - T_{ambient}) \times \text{Hours} / (ElecEff * 3,412)$$

Electric-fueled storage water heater only

Unit Peak kW Savings = Unit kWh Savings per Year / Hours
Electric-fueled storage water heater only

Unit Dth Savings per Year =
$$(A_{base} / R_{base} - A_{insul} / R_{insul}) \times (T_{hot} - T_{ambient}) \times \text{Hours} / (GasEff * 1,000,000)$$

Gas-fueled storage water heater only

TRM	R _{BASE}	R _{INSUL}	% of MN Savings	Source
MN	12	18	100%	PA TRM for R _{BASE} , 2020 online research shows R6 added is typical
Mid-Atl	8	18	250%	VEIC review for R _{BASE} , assume R8 added
PA	12	20	120%	Conservative est. of R-12 for R _{BASE} , assume R8 added.
IA	14	24	107%	None
VT	12	22	136%	None
Others	Actual			

Lighting controls

- Previous: occupancy and daylighting only, from older IL TRM
- New: Updated SF for those, plus:
 - Personal tuning
 - Task tuning
 - Multiple
 - Networked lighting controls (NLC)
- Also note and subtract baseline control savings
- SFs from:
 - 2011 LBNL meta analysis (88 studies)
 - 2017 DLC study on NLC (114 buildings)
 - Seventhwave / Slipstream work on task tuning
- Building-level available for many, but average presented too

Line voltage smart thermostats

Algorithm + baseline

- $\Delta\text{kWh} = [\text{Heating kWh of home}] \times \text{HSF} / [\text{Deemed # of t-stats per home}]$
- Get [Heating kWh of home] from RECS
 - Census Division 4 (IA, KS, MN, MO, NE, ND, SD)
 - SF detached and attached for SF, MF 2-4 and MF 5+ for MF
 - Built-in electric units installed in walls, ceilings, basements, or floors
 - Normalized Division 4 kWh by HDD to produce MN zones estimate

Zone	Baseline Baseboard Heater Household kWh	
	Single family	Multifamily
Zone 1 (Northern MN)	14,184	3,357
Zone 2 (Central MN)	12,824	2,906
Zone 3 (Southern MN/Twin Cities)	11,527	2,612

- Compare to 17,974 kWh for 2.3 tons heating
(mean MN Power HP size, TRM EFLH, HSPF = 3.412)
- [Deemed # of t-stats per home] = 6 for SF, 4 for MF
from 2017 WA State paper, root source RTF

Line voltage smart thermostats

Heating savings fraction

- Deeming **HSF** is difficult
- Possible savings from bimetallic → electronic sensor upgrade
 - Electronic / thermistor sensor may produce savings over bimetallic even if manual control before and after (reduced deadband and droop)
 - Possibly more true for line voltage than low voltage
 - Evidence for this is mixed, 0% - 7% from 2 studies
- Certainly savings from manual → smart control upgrade
 - But no studies of this upgrade for line voltage thermostats
- Other studies of low-voltage thermostats:
 - Mixed to smart, electric, coastal: 10% to 12% savings
 - Mixed to smart, gas, upper Midwest: 5% to 7% savings
 - Manual to smart, gas, upper Midwest: 9% to 13% savings
 - Programmable to smart, gas, upper Midwest: 3% savings (1 study)
- RTF uses 5% (elec sensing) + 1% (smart) = 6%
- Current recommendation: HSF = 10%

ECM fan motors

Current measure

- NOT furnace fan motors; those follow separate rule and must be ECM
- NOT 1 - 200 hp motors; those are the C/I Motors measure and follow NEMA / EPACT standards (Appendix C)
- This is an “...electronically commutated motor (ECM) being applied within fan-powered terminal boxes, fan coils, and HVAC supply fans on small unitary equipment.”
- Current MN form: $\Delta\text{kWh} = \text{CFM} \times [\text{Box Size Factor}] * \text{HOU}$
 - HOU = standard commercial EFLH
 - BSF = 0.32 W/CFM if $< 1,000$ CFM
= 0.21 W/CFM if $\geq 1,000$ CFM
 - Algorithm and factors from MA TRM, which cites “engineering analysis developed at National Grid” (no link or title, cannot find)

ECM fan motors

Possible updates

- 2018 MN Energy code, following 2018 IECC, requires motors equal to or larger than 1/12 hp (82 W) and less than 1 hp (746 W) must be ECMS or have an efficiency of 70%.
 - If 2018 MN Energy code should be followed, this measure is Replace Working only; no New Construction or Replace on Fail
 - Note 2015 MN Energy code follows 2012 IECC and does not require this
- Add exhaust
 - Only other TRM with this application is WI, which uses lighting HOU for “occupied ventilation” – will research more but this may be best option
 - Plus 8,760 for 24/7 ventilation
- Other algorithms
 - If Replace Working only, less need to make algorithm more robust, but...
 - PA: W_{BASE} and W_{EFF} are user inputs, or hp + assumed efficiency, EFLH
 - WI: hp is user input + assumed efficiency, EFLH or lighting HOU
 - NY: W_{BASE} is user input, assumed efficiency upgrade, EFLH or lighting HOU

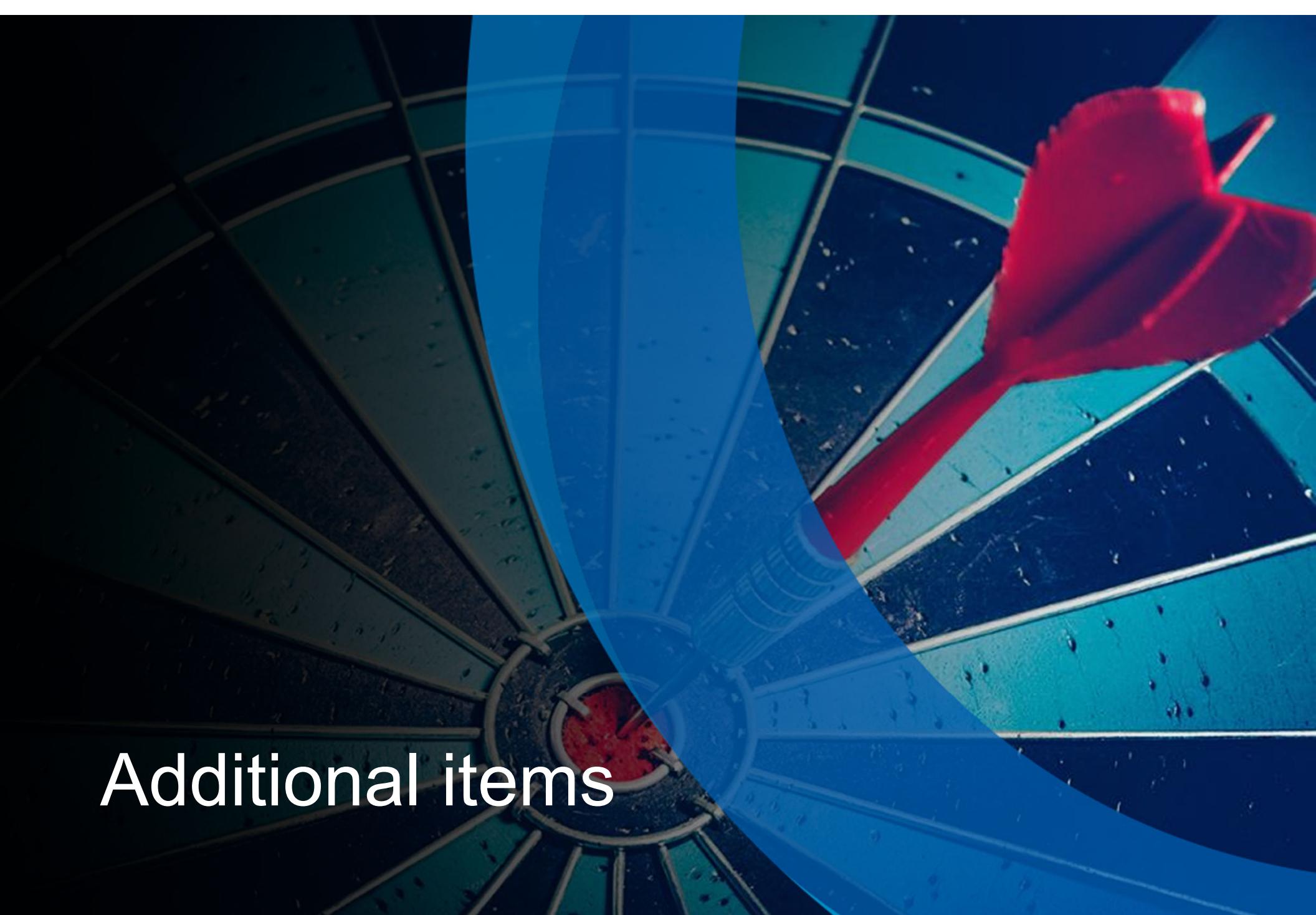
Evap fan ECMs, speed controls

Algorithm forms

- $\Delta kW_{ECM} = (W_{BASE} - W_{EE}) \times [Load Factor] \times [Duty Cycle] \times (1 + 1/COP) \times CF$
- $\Delta kW_{CTRLS} = (W_{FULL} \times \%_{FULL} - W_{LOW} \times \%_{LOW}) \times [LF] \times [DC] \times (1 + 1/COP) \times CF$
- Shaded pole, PSC, ECM, full speed, low speed wattages, other inputs from papers, data, RTF assumptions, 8,760 HOU
- Other TRMs take similar approach, using various sources

Possible update

- §431.306 requires ECM or 3-phase for evap fan motors < 1 hp & < 460 V
 - Will parse against algorithms and update shortly
- Btu/Wh requirements (via Annual Walk-In Energy Factor or AWEF) were updated 7/10/2020
 - Seven walk-in cooler types + sizes, AWEF scales with capacity
 - Believe still room for motor upgrades



Additional items

Boiler baselines

- Residential and res-sized commercial boilers, < 300 kBtu/h
- Federal code, [10 CFR Part 430](#):
 - Made before 9/1/2012: 80% AFUE
 - Made 9/1/2012 - 1/14/2021: 82% AFUE (MN TRM 3.0, 3.1 value)
 - Made on or after 1/15/2021: 84% AFUE - noted in C+S workbook in 2018
- MN TRM 3.2 applies 1/1/2022
 - This is one year of sell-through
 - Apply 84% AFUE for 3.2 (?)
- Future note, [10 CFR Part 431](#):

Boiler type, size (kBtu/h)	Current Code / TRM	Code on 1/10/2023
Hot water $\geq 300, \leq 2,500$	80% TE	84% TE
Hot water $> 2,500$	82% CE	85% CE
Steam natural draft, $\geq 300, \leq 2,500$	77% TE	81% TE
Steam natural draft, $> 2,500$		82% TE
Steam except nat draft, $\geq 300, \leq 2,500$	79% TE	81% TE
Steam except nat draft, $> 2,500$		82% TE

Apply for 2024 - 2026
Triennial? One year of
sell-through.

Other items

- Res ASHP: $SEER_{BASE}$ 13, $HSPF_{BASE}$ 7.7 → 14 and 8.2
- Commercial lighting: Hope to add new lighting types
- Correct a few references
- Correct / clarify some equation parentheses and examples
 - Steam traps
 - Insulation
 - Air purifiers
- Add clarification to terms in the energy recovery ventilator paper, small tweak to values
- Will be noted in TRM front table, also posted to Huddle with tracked changes for easy comparison

Water kWh factor

- Perhaps around 0.005 kWh / gal for MN
- Likely ~5 - 20% adder for aerator measures
- Likely < 1% adder for CIP
- Unclear path to determining factor for MN
- No issues raised regarding single factor applied, even if water source in one territory and water use in another?
- Continue to keep in mind



Thank You!